

# Second-order time-reassigned synchrosqueezing: Application to Draupner wave analysis

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# Purpose of this work

### Goals

- Computing efficient representations for handling non-stationary multicomponent signals
- Dealing with impulsive-like and/or strongly modulated signals
- Reversible representation allowing an extraction of the elementary signal components
- Meaningful information extraction from observation

⇒ **Proposed approach:** Time-frequency analysis combined with reassignment-based post-processing methods (i.e. synchrosqueezing)

Context of our research: the ASTRES project 2014-2017 funded by the French ANR

**ASTRES:** Analysis, Synthesis and Transformation by Reassignment, EMD and Synchrosqueezing.



Offers a new toolbox for non-stationary multicomponent signal processing: https://github.com/dfourer/ASTRES\_toolbox

D. Fourer, J. Harmouche, J. Schmitt, T. Oberlin, S. Meignen, F. Auger and P. Flandrin. The ASTRES Toolbox for Mode Extraction of Non-Stationary Multicomponent Signals. Proc. EUSIPCO 2017, Aug. 2017. Kos Island, Greece.

## The new French ANR ASCETE project: 2019-2022

**ASCETE:** Analysis and Separation of Complex signal: Exploiting the Time-frequency structurE



Project holder: Sylvain Meignen (LJK, Grenoble)

- Extends the previous methods with stochastic models
- Combines signal processing methods with machine learning
- New applications to audio, biomedicine, astrophysics, etc.

# Plan



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# STFT definitions

• We define the STFT of a signal x as a function of time t and frequency  $\omega$  computed using a differentiable analysis window h as:

$$F_{x}^{h}(t,\omega) = \int_{\mathbb{R}} x(\tau) h(t-\tau)^{*} e^{-j\omega\tau} d\tau$$
(1)

with  $j^2 = -1$  the imaginary unit and  $z^*$  the complex conjugate of z.

- A time-frequency representation is provided by the spectrogram defined as:  $|F_x^h(t,\omega)|^2$ .
- Signal reconstruction formula:

$$x(t) = \frac{1}{2\pi h(0)^*} \int_{\mathbb{R}} F_x^h(t,\omega) \,\mathbf{e}^{j\omega t} d\omega \tag{2}$$

when  $h(0) \neq 0$ 

## The reassignment method [Kodera et al. 1978] [Auger, Flandrin, 1995]

### Principle

Improves the readability of a time-frequency representation (TFR): Reassignment moves the signal energy according to:  $(t, \omega) \mapsto (\hat{t}_{x(t,\omega)}, \hat{\omega}_{x(t,\omega)})$ , where  $\hat{t}_x(t, \omega)$  is a group-delay estimator and  $\hat{\omega}_x(t, \omega)$  is an instantaneous frequency estimator.

Both time-frequency reassignment operators can be computed as follows (STFT case):

$$\hat{t}_{x}(t,\omega) = \operatorname{Re}\left(\tilde{t}_{x}(t,\omega)\right), \text{ with } \tilde{t}_{x}(t,\omega) = t - \frac{F_{x}^{\mathcal{T}h}(t,\omega)}{F_{x}^{h}(t,\omega)}$$
 (3)

$$\hat{\omega}_{x}(t,\omega) = \operatorname{Im}\left(\tilde{\omega}_{x}(t,\omega)\right), \text{ with } \quad \tilde{\omega}_{x}(t,\omega) = j\omega + \frac{F_{x}^{\mathcal{D}h}(t,\omega)}{F_{x}^{h}(t,\omega)}$$
(4)

where  $\mathcal{T}h(t) = th(t)$  and  $\mathcal{D}h(t) = \frac{dh}{dt}(t)$  are modified versions of the analysis window h. The reassigned spectrogram is computed by:

$$\mathsf{RF}_{x}^{h}(t,\omega) = \iint_{\mathbb{R}^{2}} |F_{x}^{h}(\tau,\Omega)|^{2} \delta\left(t - \hat{t}_{x}(\tau,\Omega)\right) \delta\left(\omega - \hat{\omega}_{x}(\tau,\Omega)\right) \mathrm{d}\tau \mathrm{d}\Omega.$$
(5)

The resulting reassigned spectrogram  $RF_x(t, \omega)$  is a sharpened but non-reversible TFR due to the loss of the phase information.

Introduction

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# The reassigned spectrogram

$$R_{x}(t,\omega) = \iint_{\mathbb{R}^{2}} \left| F_{x}^{h}(\tau,\Omega) \right|^{2} \delta(t-\hat{t}(\tau,\Omega)) \delta(\omega-\hat{\omega}(\tau,\Omega)) d\tau \frac{d\Omega}{2\pi}$$
(6)  

$$\int_{\mathbb{R}^{2}}^{\text{Spectrogram SNR=45.00 dB, L=15.01}} \int_{0}^{0} \int_{0}^{\frac{1}{2}} \int_{0}^{\frac{$$

# Synchrosqueezing [Daubechies 1996, 2011] [Thakur 2011]

### Principle

A variant of the reassignment method to compute sharpen and reversible TFRs by reassigned the transform instead of its energy to preserve the phase information.

Computation of the synchrosqueezed STFT:

$$S_{x}(t,\omega) = \frac{1}{h(0)} \int_{\mathbb{R}} F_{x}^{h}(t,\Omega) \delta(\omega - \hat{\omega}(t,\Omega)) \frac{d\Omega}{2\pi}$$
(7)

Its signal reconstruction formula:

0.45

0.35 0.3 0.2 0.2 0.2

0.1

0.05

100

150

200

time samples



100

150

200

250

time samples

400

450

500

0.

0.05

450

### Mode extraction

### Principle

Apply a time-frequency mask over a previously computed reversible TFR.  $\Rightarrow$  Performs better if the components are sparse and well disentangled.

[Brevdo, 2011] method finds the best frequency curve  $\Omega(t)$  to maximizes the energy with a smooth constraint through a total variation penalization term:

$$\hat{\Omega} = \underset{\Omega}{\operatorname{argmax}} \int_{\mathbb{R}} |S_{\mathsf{x}}(t, \Omega(t))|^2 dt - \lambda \int_{\mathbb{R}} \left| \frac{d\Omega}{dt}(t) \right|^2 dt, \qquad (9)$$

where  $\lambda$  controls the importance of the smoothness of  $\Omega$ .

<u>Notice</u>: When the ridges of several components have to be estimated, this method can be iterated after subtracting the energy located at the previously estimated ridge.

Rationale Second-order time-reassigned synchrosqueezing

## STFT properties

The STFT marginalization over time of  $F_x^h(t,\omega)$  leads to:

$$\int_{\mathbb{R}} F_{x}^{h}(t,\omega) dt = \iint_{\mathbb{R}^{2}} h(t-\tau)^{*} x(\tau) e^{-j\omega\tau} dt d\tau$$
(10)

$$= \iint_{\mathbb{R}^2} h(u)^* x(\tau) \, \mathbf{e}^{-j\omega\tau} \, du d\tau \tag{11}$$

$$= \int_{\mathbb{R}} h(u)^* du \int_{\mathbb{R}} x(\tau) \, \mathbf{e}^{-j\omega\tau} d\tau \qquad (12)$$

$$=F_h(0)^*F_x(\omega) \tag{13}$$

with  $F_x(\omega) = \int_{\mathbb{R}} x(t) e^{-j\omega t} dt$  the Fourier transform of signal x. Hence, the signal can be recovered by:

$$x(t) = \frac{1}{2\pi F_h(0)^*} \iint_{\mathbb{R}^2} F_x(\tau, \omega) \,\mathbf{e}^{j\omega t} \,d\tau d\omega \tag{14}$$

Rationale Second-order time-reassigned synchrosqueezing

## Time-reassigned synchrosqueezed STFT [He 2019]

### Principle

Synchrosqueezes the original transform along the time axis instead of the frequency axis exploiting the STFT properties when marginalized over time.

The time-reassigned synchrosqueezed STFT can be defined as:

$$T_{x}^{h}(t,\omega) = \int_{\mathbb{R}} F_{x}^{h}(\tau,\omega) \delta\left(t - \hat{t}_{x}(\tau,\omega)\right) d\tau$$
(15)

where  $\hat{t}_x(t,\omega)$  corresponds to a group-delay estimator related to the time reassignment operator given by Eq. (3).

The original signal can thus be reconstructed using the following exact formula:

$$x(t) = \frac{1}{2\pi F_h(0)^*} \iint_{\mathbb{R}^2} T_x^h(\tau, \omega) \, \mathbf{e}^{j\omega t} \, d\tau d\omega \tag{16}$$

#### Rationale

Second-order time-reassigned synchrosqueezing

## Numerical results



- Perfect localization of the 2 impulses
- Poor localization of the sinusoidal components

Signal model

$$x(t) = \mathbf{e}^{\lambda_{\mathbf{x}}(t) + j\phi_{\mathbf{x}}(t)}$$
(17)

Second-order time-reassigned synchrosqueezing

with 
$$\lambda_{x}(t) = l_{x} + \mu_{x}t + \nu_{x}\frac{t^{2}}{2}$$
 (18)

Rationale

and 
$$\phi_x(t) = \varphi_x + \omega_x t + \alpha_x \frac{t^2}{2}$$
 (19)

where  $\lambda_x(t)$  and  $\phi_x(t)$  respectively stand for the log-amplitude and phase and with  $q_x = \nu_x + j\alpha_x$  and  $p_x = \mu_x + j\omega_x$ .

For such a signal, it can be shown that [Fourer et al., 2017]:

$$\omega_{x} = \operatorname{Im}(\tilde{\omega}_{x}(t,\omega) - q_{x} \tilde{t}_{x}(t,\omega)) = \hat{\omega}_{x}(t,\omega) - \operatorname{Im}(q_{x} \tilde{t}_{x}(t,\omega))$$
(20)

Rationale Second-order time-reassigned synchrosqueezing

### Enhanced group-delay estimation

The new proposed second-order horizontal synchrosqueezing consists in moving  $F_x^h(t,\omega)$  from the point  $(t,\omega)$  to the point  $(t_x^{(2)},\omega)$  located on the instantaneous frequency curve, *i.e.* such that  $\dot{\phi}(t_x^{(2)}) = \frac{d\phi_x}{dt}(t_x^{(2)}) = \omega_x + \alpha_x t_x^{(2)} = \omega$ .

This leads to:

$$t_{x}^{(2)} = \frac{\omega - \omega_{x}}{\alpha_{x}} = \hat{t}_{x}(t,\omega) + \frac{\omega - \hat{\omega}_{x}(t,\omega)}{\alpha_{x}} + \frac{\nu_{x}}{\alpha_{x}} \operatorname{Im}(\tilde{t}_{x}(t,\omega))$$
(21)

which can be estimated by:

$$\hat{t}_{x}^{(2)}(t,\omega) = \begin{cases} \frac{\omega - \hat{\omega}_{x}(t,\omega) + \operatorname{Im}(\hat{q}_{x}(t,\omega) \ \tilde{t}_{x}(t,\omega)))}{\hat{\alpha}_{x}(t,\omega)} & \text{if } \hat{\alpha}_{x}(t,\omega) \neq 0\\ \hat{t}_{x}(t,\omega) & \text{otherwise} \end{cases}$$
(22)

where  $\hat{q}_{x}(t,\omega) = \hat{\nu}_{x}(t,\omega) + j\hat{\alpha}_{x}(t,\omega)$  is an unbiased estimator of  $q_{x}$ .

Rationale Second-order time-reassigned synchrosqueezing

### Implementation considerations

In [Fourer et al., 2017] and [Fourer et al., 2018] we introduced two families of unbiased estimators called (tn) and  $(\omega n)$  involving *n*-order derivatives  $(n \ge 2)$  with respect to time (resp. to frequency) which enable to compute Eqs. (22).

$$\hat{q}_{x}^{(tn)}(t,\omega) = \frac{F_{x}^{\mathcal{D}^{n}h}F_{x}^{h} - F_{x}^{\mathcal{D}^{n-1}h}F_{x}^{\mathcal{D}h}}{F_{x}^{\mathcal{T}h}F_{x}^{\mathcal{D}^{n-1}h} - F_{x}^{\mathcal{T}\mathcal{D}^{n-1}h}F_{x}^{h}}$$
(23)

$$\hat{q}_{x}^{(\omega n)}(t,\omega) = \frac{(F_{x}^{\mathcal{T}^{n-1}\mathcal{D}h} + (n-1)F_{x}^{\mathcal{T}^{n-2}h})F_{x}^{h} - F_{x}^{\mathcal{T}^{n-1}h}F_{x}^{\mathcal{D}h}}{F_{x}^{\mathcal{T}^{n-1}h}F_{x}^{\mathcal{T}h} - F_{x}^{\mathcal{T}^{n}h}F_{x}^{h}}$$
(24)

with  $\mathcal{D}^n h(t) = \frac{d^n h}{dt^n}(t)$  and  $\mathcal{T}^n h(t) = t^n h(t)$ .

- discrete-time reformulations of our previously described expressions combined with the rectangle approximation method. Thus  $F_x^h[k,m] \approx F_x^h(\frac{k}{F_s}, 2\pi \frac{mF_s}{M})$ , where  $F_s$  denotes the sampling frequency,  $k \in \mathbb{Z}$  is the time sample index and  $m \in \mathcal{M}$  is the discrete frequency bin.
- The number of frequency bins M is chosen as an even number such as  $\mathcal{M} = [-M/2 + 1; M/2]$
- Our implementation uses a Gaussian window expressed as  $h(t) = \frac{1}{\sqrt{2\pi}T} e^{-\frac{t^2}{2T^2}}$ where T is the time-spread of the window which can be related to  $L = TF_s$ .

Rationale Second-order time-reassigned synchrosqueezing

# Comparative numerical results 1/2



Rationale Second-order time-reassigned synchrosqueezing

## Comparative numerical results 2/2



Rationale Second-order time-reassigned synchrosqueezing

# Signal reconstruction

Whole signal reconstruction expressed in terms of Reconstruction quality Factor (RQF):

$$RQF = 10 \log_{10} \left( \frac{\sum_{n} |x[n]|^2}{\sum_{n} |x[n] - \hat{x}[n]|^2} \right)$$
(25)

Method	RQF (dB)
STFT	269.27
reassignment	N/A
classical synchrosqueezing	35.89
second-order vertical synchrosqueezing	23.80
time-reassigned synchrosqueezing	116.67
second-order time-reassigned synchrosqueezing	116.67

Data description Application to Draupner wave analysis

### Draupner wave recording

We consider a possible freak wave event measured in the North Sea on the Draupner Platform the 1st of january 1995.



Data description Application to Draupner wave analysis

## Draupner wave signal [Haver, 2004]

- The signal corresponds to the sea surface elevation deduced from the measures provided by a wave sensors consisting of a down-looking laser.
- The sampling frequency of this signal is  $F_s = 2.13$  Hz and the duration is 20 minutes.



#### Data description Application to Draupner wave analysis

## Time-frequency representations



Data description Application to Draupner wave analysis

### Impulses detection

### Proposed Saliency function

Defined as the root mean square of the marginal over frequency band  $\Omega = [0.4; 1]$  Hz of the signal energy contained in the considered time-frequency representation.

$$G(t) = \left(\int_{\Omega} |TFR_{x}^{h}(t,\omega)|^{2} d\omega\right)^{\frac{1}{2}}.$$
 (26)



Figure : Result provided using the second-order horizontal synchrosqueezing.

Data description Application to Draupner wave analysis

# Impulses disentangling

A binary masked version of the transform  $S_x^h(t,\omega)$  can thus be computed using G(t) as:

$$\hat{S}(t,\omega) = \begin{cases} S_x^h(t,\omega) & \text{if } G(t) > \Gamma \\ 0 & \text{otherwise} \end{cases}$$
(27)

where  $\Gamma$  is a defined threshold.

Our numerical computation uses  $\Gamma = 3.37$  which corresponds to 5 times the mean value of G(t).



Figure : Draupner signal and recovered waveform of its impulsive components.

## Contributions summary

- A novel horizontal synchrosqueezing method based on an enhanced group-delay estimator.
- Efficient computation from the STFT using specific analysis windows.
- New applicative results based on the Draupner wave signal.

Matlab code freely available on IEEE Code Ocean at: http://fourer.fr/hsst